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Geophysical Exploration Report
Highland Horizon Pool
Brushy Creek Municipal Utility District

February 16, 2026

Prepared for:

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President

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REPORT INDEX

APPENDIX A – GEOPHYSICAL DATA

Geophysical Exploration Report
Brushy Creek Municipal Utility District
Williamson County, Texas

A. INTRODUCTION

Zara Environmental, LLC. engaged Gehrig, Inc. to perform a geophysical investigation at the Highland Horizon Pool in the Brushy Creek Municipal Utility District (MUD) outside of Austin, Texas. The primary objective is to detect and delineate potential significant karst features, if present, below inground pool shells. Ensor Cave is present immediately southwest of the pool area in question. A detailed plan and profile view of the cave has been provided for review [2]. Cracking of the pool shells developed on the east end of the kids (west) pool and on the west end of the deeper adult (east) pool. The cracks had been repaired at the time of our investigation. An approximate 2 foot wide barrier separates the two inground pool shells.

Gehrig, Inc. proposed two exploration geophysical methods to meet the project objective, specifically ground penetrating radar (GPR) and microgravity to provide a more detailed analysis of subsurface conditions. On February 3 and 4, 2026, Gehrig, Inc. collected field geophysical measurements. GPR provided a more rapid reconnaissance of subsurface conditions. Microgravity stations were positioned in and around the pool area. Microgravity readings were also extended around the Ensor Cave area to better track this cave system from the surface.

This report should be used in conjunction with all other relevant subsurface information acquired across this project area in establishing surface and subsurface conditions. This report should not be construed as a warranty of surface or subsurface conditions.

B. DOCUMENTATION REVIEW

I. Regional Geologic Conditions

Based on the Geologic Atlas of Texas, Austin sheet [1], the site is situated within the Edwards Limestone Formation (Ked) of the Cretaceous geologic age. The Edwards Limestone Formation consists of limestone, dolomite, and chert. The formation thickness is typically 60 to 350 feet and is medium gray to grayish brown in color. Fossils are rudistids as reef and individuals, miliolids, and shell fragments with abundant solution zones and collapse breccia are common. Edwards Limestone is highly karstified with sinkholes, cave, conduits, and springs.

C. NEAR SURFACE GEOPHYSICAL EXPLORATION TECHNIQUES

Near surface geophysical exploration techniques are typically defined as exploratory techniques for the upper 100+ feet. Geophysical methods provide relatively non-destructive means of assessing subsurface conditions. There are several near surface geophysical techniques which can be implemented, namely seismic reflection and refraction, multi-channel analysis of surface waves (MASW), ground penetrating radar (GPR), electrical resistivity tomography (ERT) and induced polarization (IP), electromagnetic mapping (tTEM), gravity, and magnetic surveying. Each technique has its pros and cons based on given subsurface geologic conditions, project scope, economics, etc. Further, geophysical techniques can be used to better identify points or areas of further testing, i.e., test pits, geotechnical borings, hydrogeological test wells, etc.

By the very nature of geophysical exploration techniques, acquired data has an inherit depth uncertainty in comparison to more destructive exploration techniques such as geotechnical borings or test pit excavation. *It should be stated that estimated depths with geophysical exploration techniques cannot be construed as exact depth measurements.*

D. GROUND PENTETRATING RADAR (GPR)

I. General Description

Ground Penetrating Radar (GPR) is a short pulse of electromagnetic energy, which is radiated into the subsurface. When this pulse strikes an interface between layers of materials with different electrical properties, part of the wave reflects, and the remaining energy continues to the next interface. Ground penetrating radar is very useful in determining concrete section depth, reinforcement bar placement, post-tension cable placement, and the spatial location of void spaces beneath the concrete slab. Subsurface void detection with GPR is possible due to the dielectric contrast between air and the surrounding soils. For an air-filled void, the GPR response is typically a strong, negative polarity signal return on the radargram. For a water filled cavity, the GPR response is typically a strong, positive polarity signal return on the radargram.

II. Equipment and Methods

A GS9000 pushcart GPR system manufactured by Proceq was used for the GPR survey. The antenna accompanying the GS9000 system is Proceq's GX2 multi-channel array module with a modulation range of 30-750 MHz across 11 (VV) channels. The GX2 antenna's frequency range is designed to provide a comprehensive view of the upper 10 feet below ground surface (BGS), which is a well-suited depth range for this application. Proceq's iOS field app (GS), which runs on an iPad Pro tablet, controlled the operations of the GPR equipment for data acquisition. An integrated MA8000 GNSS receiver allowed for georeferencing of the entire GPR survey. The GPS receiver utilizes Space State Representation (SSR) correction services which is capable of tracking multiple satellite constellations and delivers sub-decimeter accuracy for the location of each GPR linescan.

A Proceq GP8100 high-resolution (HiRes), multi-antenna concrete GPR array was also deployed for rapid, detailed subsurface imaging. It uses stepped-frequency continuous-wave (SFCW) radar across a 400–4000 MHz frequency range, enabling both fine-detail resolution and practical penetration (up to ~30 inches in concrete). With six antennas, a 10 inch effective scan width, and a 1,200 scans/second acquisition rate, it produces dense, high-clarity data in a single pass—equivalent to multiple traditional line scans. The system is compact, lightweight, and optimized for fast object detection, rebar mapping, and structural assessment. The main purpose of this antenna is to located any voids directly below the gunite pool shell.

The main performance limitation for GPR is the presence of fine-grained soils, high salt content soils, and/or other low electrical resistive soils. These subsurface soil conditions can severely inhibit GPR signal penetration and imaging. Tightly spaced concrete reinforcement, i.e., welded wire mesh, can also inhibit GPR penetration depth.

E. MICROGRAVITY

I. Gravity Equipment

A Scintrex CG-6 autogravity meter was used. The CG-6 is an automated gravity meter with a resolution reading of 0.1 μGal. The relative value of gravity, *g*, is determined by a series of measurements recorded at a sampling frequency of 10 hertz (Hz). Based on individual readings and after the rejection of deviant values, the gravity meter provides the arithmetic mean, *n*, of the individual measurements and their standard deviation (SD). Assuming a normal noise distribution, the measurement error is estimated by err = SD/√n. This error incorporates the instrumental error associated with the acquisition system plus any seismic noise affecting the measurement spring at different frequencies. The device is equipped with tilt and internal temperature sensors, and the data are corrected in real time from the observed variations. These different parameters are stored in memory.

During the recording of a reading the CG6 will show variations in the calculated measurement error. These variations are generally a result of modification in the surrounding environment. Changes in the levels of the instrument can cause fluctuations on the calculated error as can passing urban traffic. Seismic and meteorological interference can also increase the error. An effective way to reduce this measurement error is to increase the duration, and consequently, the number of measurements used to calculate the error. If this is not successful, the survey should be stopped until such a time that the external effects have been reduced enough to allow the acquisition of accurate data.

II. Gravity Survey Design

Gravity measurements were typically acquired over GPR anomalies in addition to a grid covering the area of concern. Four microgravity readings were averaged over a 30 second period at each occupation to reduce errors caused by ground vibration. A base station was established near the west center of the tract. Base readings were taken at approximately 1 to 2-hour intervals.

III. Relative Site Elevation Control

The topographic information needed for the accurate reduction of microgravity data was acquired by using a Stanley Compulevel. Based on manufacturer specifications, the typical isothermal accuracy is the greater of 0.1 inch or 0.15% of the reading.

IV. Data reduction and processing

The relative measurements recorded by the gravity meter between the base station and the acquisition grid are subject to several external effects that are not related to the subsurface geology. For a valid geophysical interpretation to be made, these effects must be removed. The process of correcting for these effects is a well-established routine in any gravity survey and is often called the reduction of data. The necessary corrections are described as follows:

- **Free air correction.** This correction considers the vertical decrease in gravity with increased elevation. The correction is based on the inverse square dependence of the acceleration due to gravity on the distance from a datum plane.

- **Bouguer correction**. The free air correction accounts solely for the variation in height between gravity points. The Bouguer correction accounts for the attraction of material between reference height and that of the gravity station. This can be approximated by treating the intervening rock material as an infinite horizontal slab, of a thickness equal to the elevation difference, h, between the reference base and the gravity station, with a density of 2,450 kg/m^3.

- **Latitude correction.** Because the earth is not spherical – the equatorial radius is greater than the polar radius – a correction is needed relative to the distance northward or southward. The formula prescribed by the International Gravity Standardization Network (I.G.S.N) in 1971 to calculate the theoretical absolute gravity value was used.

- **Drift correction.** The zero-length spring used in the gravity instruments experience gradual change in reading with time. This drift is a result of the imperfect elasticity of the springs, which undergo an elastic creep with time and are unrelated to gravity changes. The correction for instrument drift is performed by the Scintrex CG-6 Autograv and corrected automatically in the output data. However, repeated base station readings throughout the site work are performed as a check on both this and the tidal correction.

- **Tidal correction**. As well as the above effects, gravity measured during a survey varies with time because of periodic variation in the gravitational effects of the sun and moon associated with their orbits. In a high precision survey these effects must be corrected. The Scintrex CG-6 autograv calculates earth tides corrections automatically.

The microgravity data was processed using a Microsoft Excel spreadsheet created inhouse. Figure 1 – Bouguer Microgravity Map plots the overall site gravity of the tract after all appropriate corrections have been made. Figure 2 - Residual

Microgravity Map assists in the removal of long wavelength, regional trends from the data by deducting a regression trend from the data set. The final data output, which includes the regression trend removal, was gridded using the Kriging method in Surfer v.28 from Golden Software, Inc.

V. General Discussion of Microgravity Results

Microgravity is the interpretation of changes in the subsurface density distribution from the measurement of minute variations in the gravitational attraction of the Earth. As a technique, it is particularly suited to the investigation of subsurface structures, mapping of geological boundaries and, most importantly in this case, the location and characterization of karsts or voids. Gravity variations due to the geological/petrophysical changes associated with fracturing and changes in pore composition are superimposed upon much larger variations due to elevation, latitude, topography, Earth tides and regional geological variations. However, these external changes can be modelled or monitored with sufficient accuracy to be removed from the data.

In general, the following observations can be generalized with regards to karst feature detection using gravity methods:

- A very low gravity anomaly is indicative of air-filled and/or spatially extensive large void(s). As an example, a 20 foot diameter air-filled spherical void with top of void ~10 feet below grade level would yield a theoretical response of -50 μGal. Very low gravity responses was recorded at this site near the cave entrance. This is represented by the dark blue colors

- A low gravity anomaly can be indicative of a smaller air filled void, less dense soils, high fractured network, and/or infilled karst terrain. This is represented by the light blue colors in Figure 2, possibly extending into the dark brown areas. As an example, a 14 foot diameter, spherical air-filled void with top of void ~10 feet below grade level would yield a theoretical response of -25 μGal.

- A near zero μGal background or positive gravity measurement is typically indicative of more intact dense soil/rock with minimal or no karst development. This is represented by the tan to brown colors in Figure 2.

For karstic terrain, a spherical void is typically not a geological reality. As shown by the Ensor Cave diagram [3], karstic terrain is highly variable with asymmetrical backrooms, chambers, boulder crawls, rock density variations (i.e. lower density pulverulite), lower density clay infills, throats, fractures, and bedding plane byway. Further, the shape, size, and depth of all these features also impacts the microgravity readings at the surface. It should be strongly emphasized that microgravity measures the totalities of these karstic influences directly below each gravity station. It reality, actual air-filled voids are typically less than the theoretical responses due to these geologic complexities of karstic terrain.

Figure 2 – Residual Microgravity Map plots the gravity trends of the site after polynomial trend analysis have been performed to minimize regional gravity trends. Based on Figure 2, very distinct, linear low gravity anomaly (i.e., -20 to -50 μGal) were recorded at this site. Further interpretation of the geophysical results will be discussed in Section G.

G. INTERPRETATION OF GEOPHYSICAL RESULTS

Of the two methods deployed, microgravity provides the more direct evidence of subsurface karst features. GPR also assisted in mapping anomalous reflective zones, which corresponded with residual gravity low feature. GPR also aided in utility mapping along the south end of the pool shells. The following provides an overall interpretation summary:

- Figure 1 - Bouguer Microgravity Map provides a regional gravity map highlighting an overall gravity gradient trending lower towards Ensor Cave system. Higher gravity readings were typically directly below the pool shell.

- Figure 2 plots the residual map with trend removal. Residual gravity provides a more detailed, site specific analysis of density variations across the site. Interpretation mark-ups are also included.

- Residual gravity map reasonably mapped out the Ensor cave system with some extensions from the known outline as shown in Figure 2. A distinct gravity low at station 54 suggests a previously unknown chamber is likely present east of the known cave system. Further, karstic terrain likely extending further north of the known cave system, albeit the gravity responses suggests it might be related to the bedding plane byway versus a large chamber. GPR reflectivity in the shallower rock units was high in this area as shown in Figures 8 to 10.

- HiRes GPR data over the pool shell did not encounter any voids directly below the gunite pool shell. Further, deeper penetrations from the 3D GS9000 unit did not record any anomalous reflectivity signal that could be attributed to karstic terrain.

- Gravity data suggests that Ensor Cave system or other karstic terrain does not extend below the inground pool shells. Gravity data suggest competent, intact limestone rock is present below the pool shell with no recorded gravity lows present. Further, the GPR data did not encounter any voids directly below the pool shells. Therefore, Gehrig, Inc. is of the opinion that the karstic topography is not responsible for cracking in the pool shell.

- Slight, isolated gravity lows were encountered below the pool decking south of the pool shells. GS9000 picked up utilities and their trenches in these areas. Backfill soils with the trenches, along with the utilities themselves, are likely responsible for these localized gravity lows. Theoretical mapping very shallow voids from utilities can yield similar responses in the upper two feet.

- The remaining site encountered normal gravity variations as represented by the brown and tan color shades in Figure 2. Some gravity variations are to be expected within the upper limestone rock mass due to spatial and vertical weathering variations, small scale vugs/cavities, and limestone rock density variations.

It should be emphasized that all formation contacts and boundaries are not exact due to the inherent nature and limitations of geophysical exploration and imaging. Subsurface features that do not produce a measurable geophysical response or those masked by other features may not be detectable. Our interpretations should be considered a general assessment of the subsurface conditions at this site based on prior geotechnical information, documentation review, and geophysical datasets. Confirmation borings are typically a logical next step to further investigate this subsurface feature. This report should not be construed as a warranty of surface or subsurface conditions.

H. PLAUSIBLE EXPLANATION FOR POOL SHELL CRACKING

Resistance to shrinking (RTS) cracking is a well-recognized issue in structural engineering community, especially where shallow bedrock is present. When a concrete foundation, such as a gunite pool shell in this case, is partly supported by solid limestone and partly by a sand subbase, shrinkage cracks can develop. It’s likely that the dividing wall between the two pool shells rests directly on limestone, while the shells themselves are supported by a subbase. Except for the southeast corner of the east pool shell, ground penetrating radar (GPR) indicated the presence of a subbase beneath the pool shell. This arrangement allows the dividing wall to remain stable, but the pool shells may ‘float’ on the subbase, leading to internal tensile stresses and shrinkage cracks. Notably, the cracks did not show vertical displacement, which is characteristic of shrinkage cracking rather than cracks caused by differential settlement. Additionally, the cracks appeared at nearly equal distances from both sides of the wall, further supporting the RTS cracking explanation.

I. REFERENCES

1. Bureau of Economic Geology, *Geologic Atlas of Texas, Austin Sheet*. Reprinted 1981.

2. American Society for Testing and Materials (ASTM) D 6430 – Guidelines for Using the Gravity Method for Subsurface Investigation.

3. Ensor Cave plan and profile views, with and without annotations, dated April 16, 2025.

J. LIMITATIONS

This investigation and report have been performed in accordance with the standard of care and skill ordinarily exercised by professionals practicing in the same locality under similar conditions at the time of the investigation. All analyses, interpretations, and/or recommendations are based solely on the geophysical data collected during the investigation period and the information provided by client. No warranty, expressed or implied, is made regarding the accuracy, completeness, or suitability of this report for any particular purpose. This report is intended for informational use only and does not constitute a guarantee or warranty as to future performance, repair needs, or suitability for any specific application.

This report is prepared exclusively for the client identified herein. Any use or reliance by third parties, or for purposes other than those expressly stated, is strictly prohibited unless prior written consent is obtained. Gehrig, Inc. expressly disclaims any liability to third parties or for unauthorized uses.

Interpretations and conclusions are based on limited geophysical data and should be considered general assessments. Subsurface conditions may vary significantly across the site and may not be fully represented by the geophysical data collected. Features not producing measurable geophysical responses or masked by other subsurface conditions may not be detectable. Confirmation borings or additional testing are recommended for rigorous evaluation. This report should not be construed as a warranty of surface or subsurface conditions.

If additional information becomes available or site conditions change after the date of this report, Gehrig, Inc. reserves the right to review and revise its analysis and conclusions, as necessary. No responsibility is accepted for the impact of such changes unless specifically requested and agreed to in writing.

The client agrees to indemnify and hold harmless Gehrig, Inc. and its affiliates from any claims, damages, or liabilities arising from unauthorized use, reliance, or distribution of this report. Under no circumstances shall Gehrig, Inc. be liable for any indirect, incidental, special, or consequential damages, including but not limited to loss of profits, business interruption, or loss of data, arising out of or in connection with the use of this report

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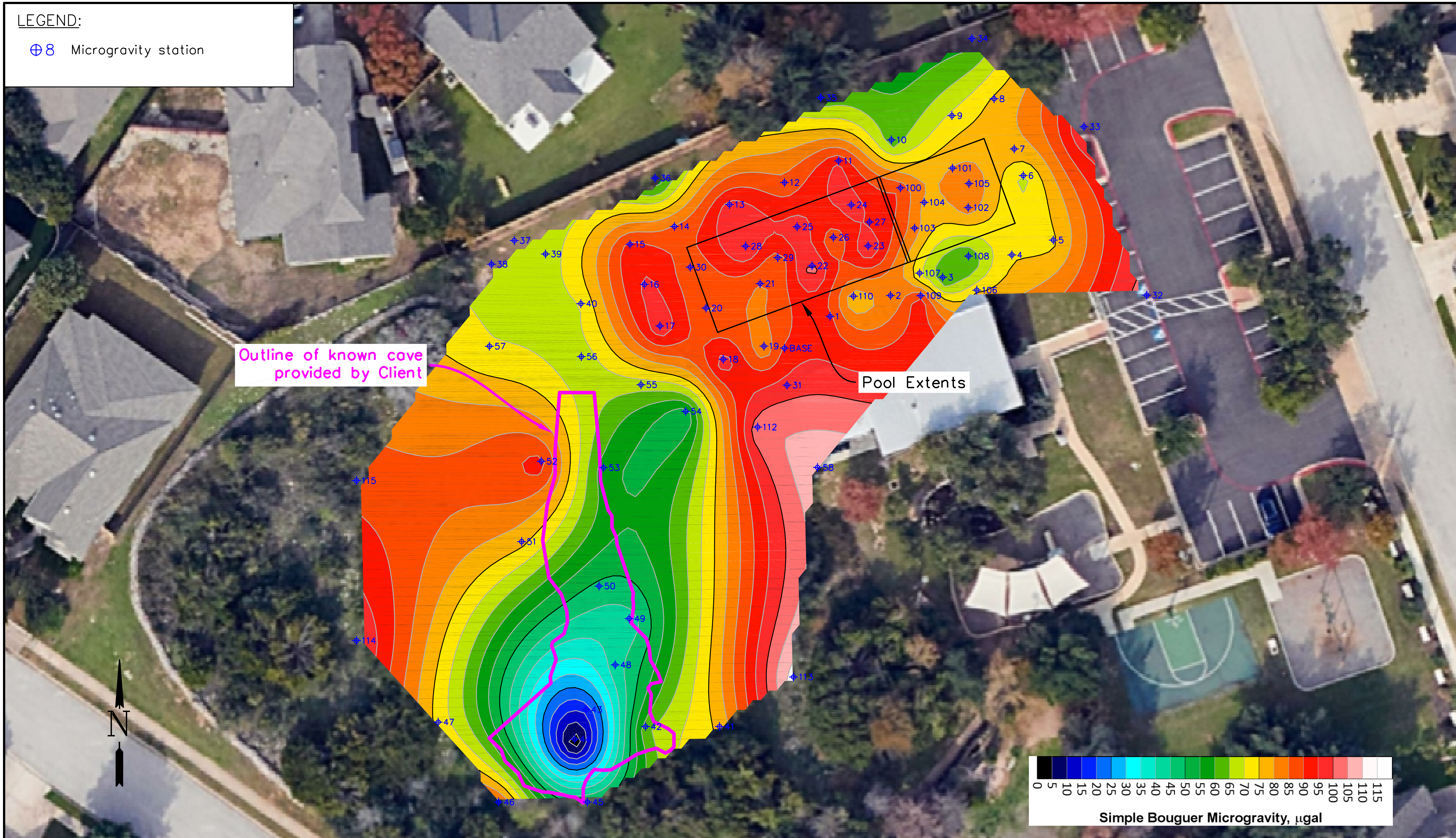

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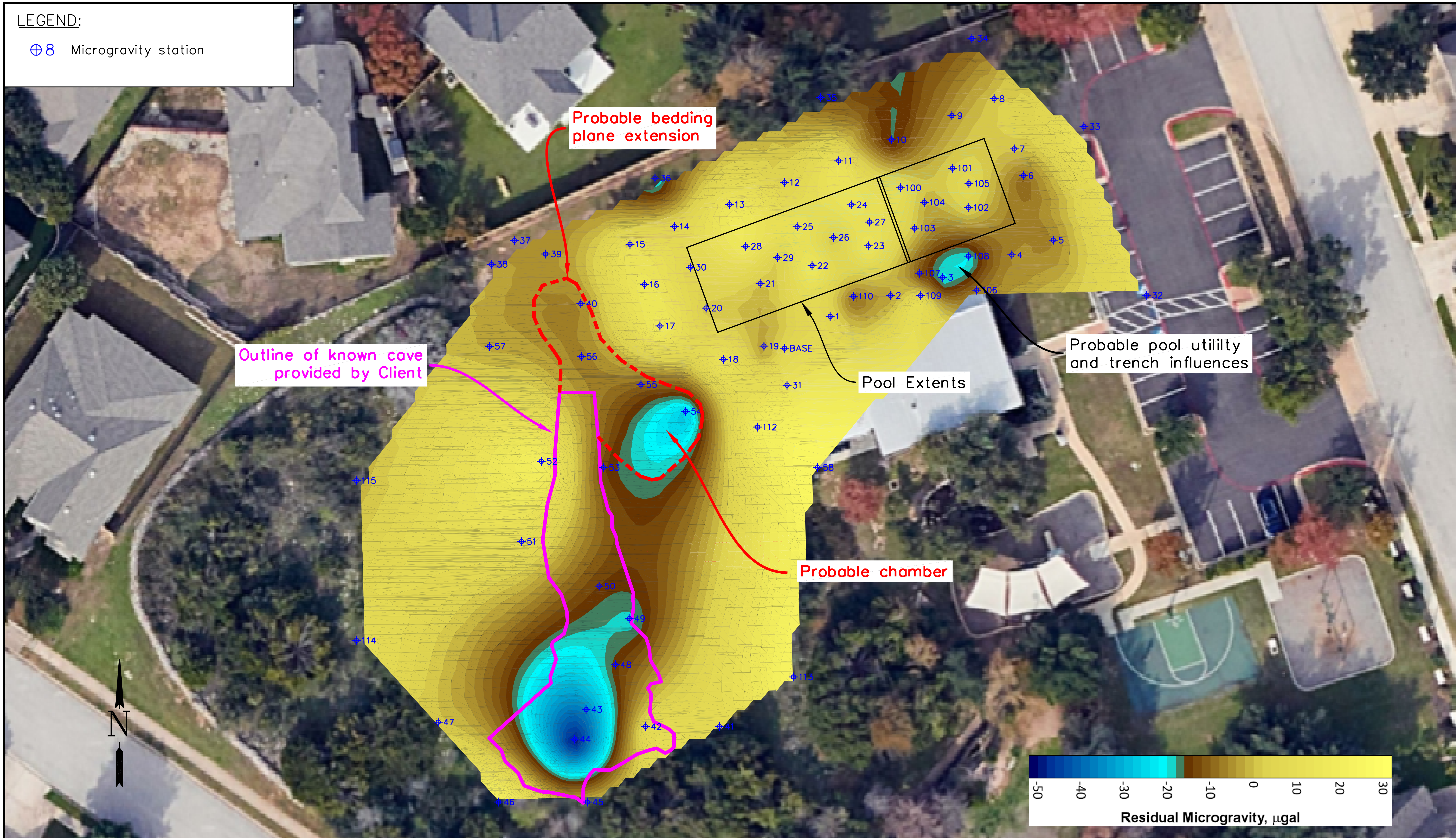
0 15 30 60
(IN FEET)
1 inch = 30 ft. Horiz.

BOUGUER GRAVITY
Highland Horizon Pool
Austin, Texas 78717
Project #: 26-10-006
Survey Date: February 3-4, 2026

ZARA ENVIRONMENTAL LLC

Notes:
1. Aerial: Google Imagery
2. Datum: State Plane Nad83 - TX Central, ft

Figure No.
1



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RESIDUAL GRAVITY

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1. Aerial: Google Imagery
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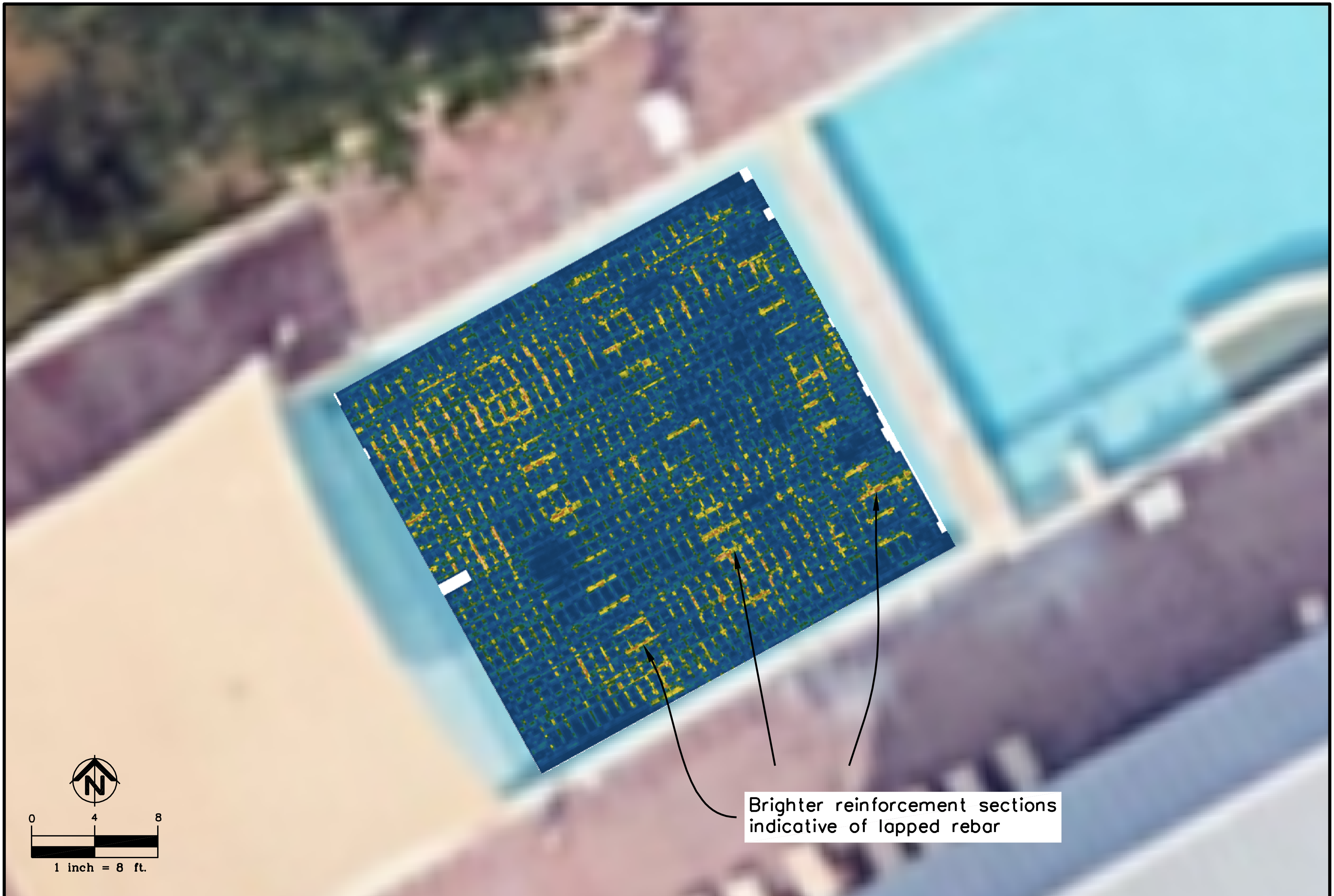
Figure No.
2



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HiRes GPR Horizontal Depth Slice - 6 inches

Highland Horizon Pool - West Pool

Austin, TX 78717

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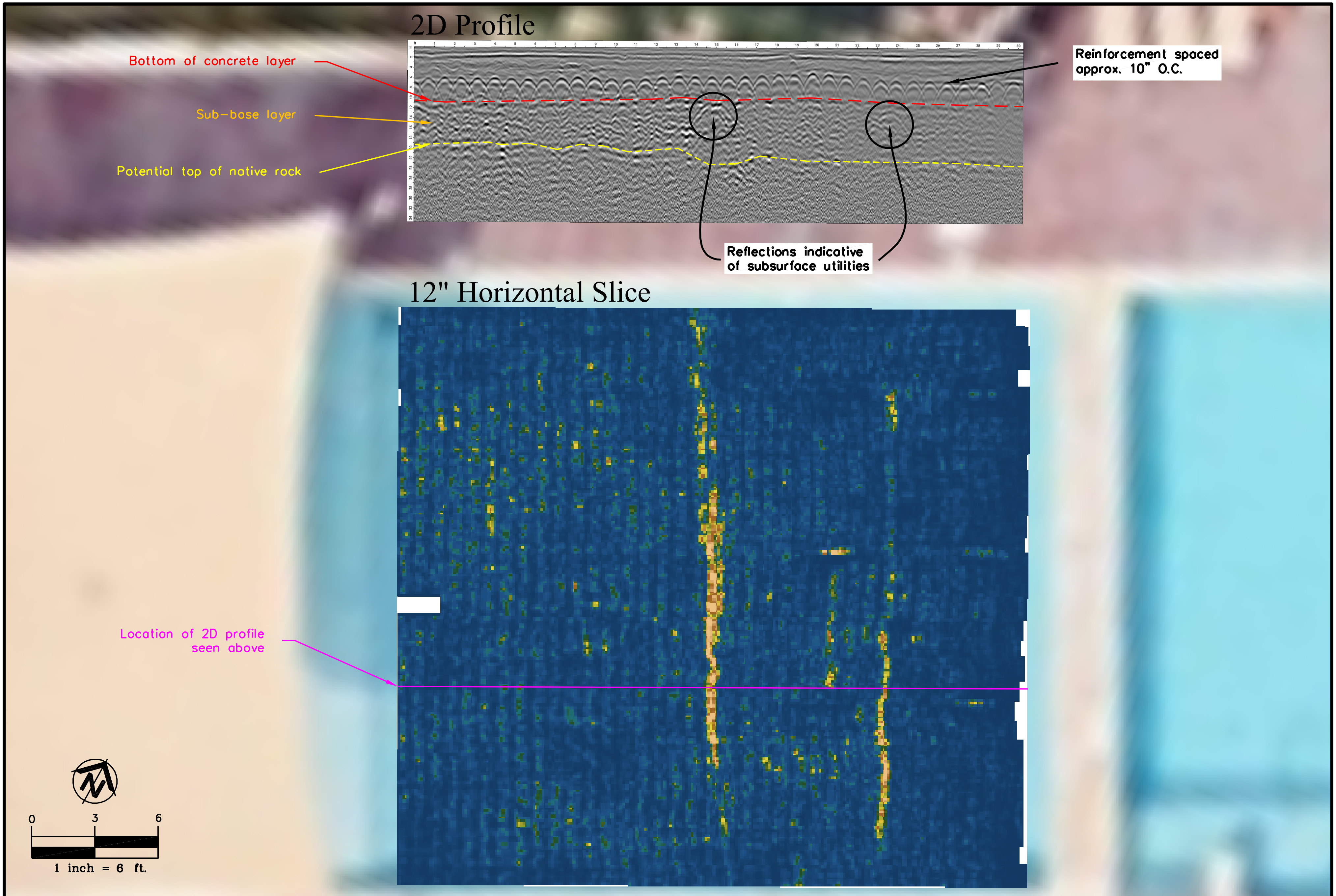
Notes:
1) Project Date: February 3-4, 2026
2) Gehrig, Inc. Project #: 26-10-006
3) GPR data collected with GP8100 antenna

Figure No. 3



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HiRes GPR Vertical Slice Example: West Pool

Highland Horizon Pool - West Pool

Austin, TX 78717

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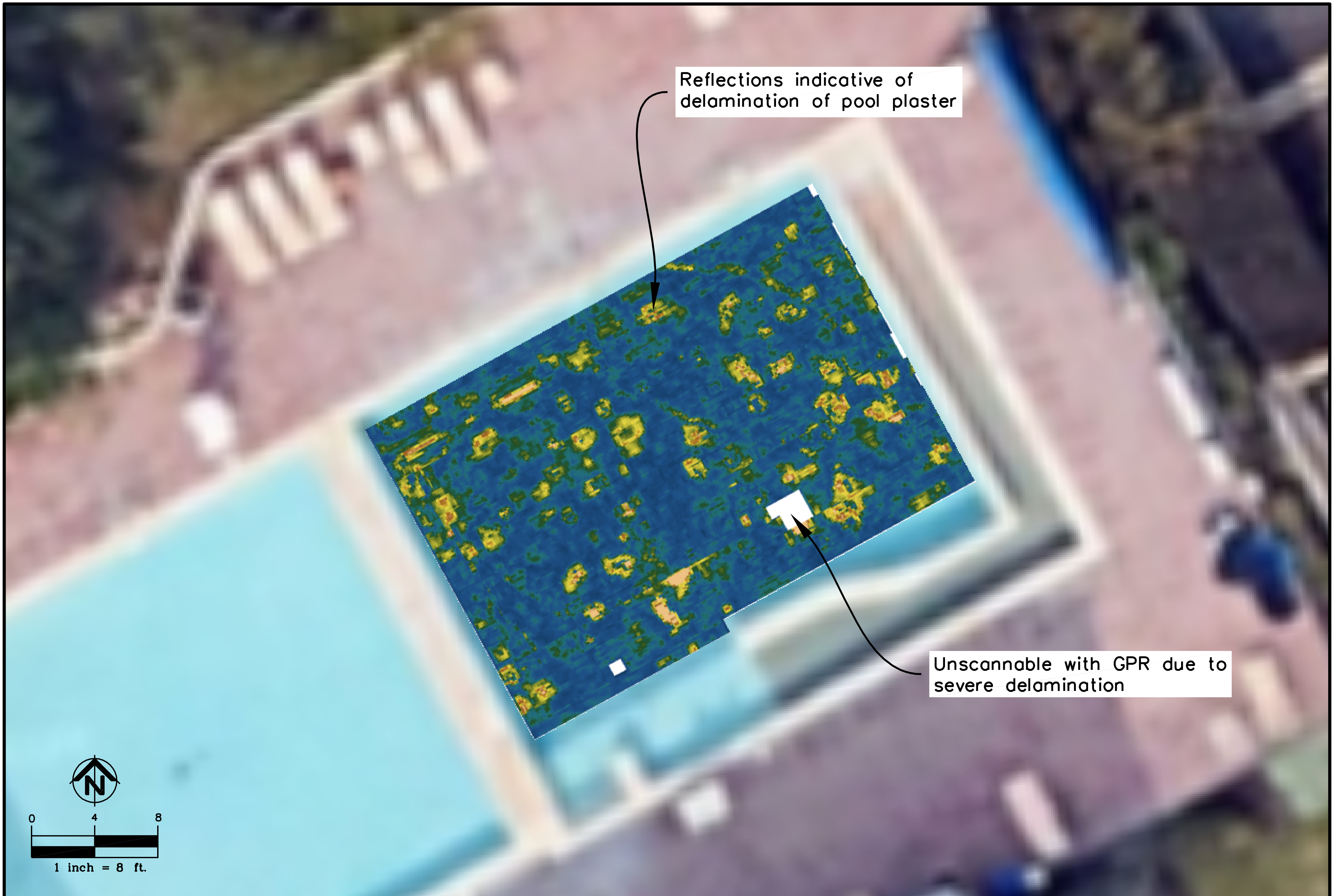
Notes:

1) Project Date: February 3-4, 2026
2) Gehrig, Inc. Project #: 26-10-006
3) GPR data collected with GP8100 antenna

Figure No. 4



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HiRes GPR Horizontal Depth Slice - 1 inch

Highland Horizon Pool - East Pool

Austin, TX 78717

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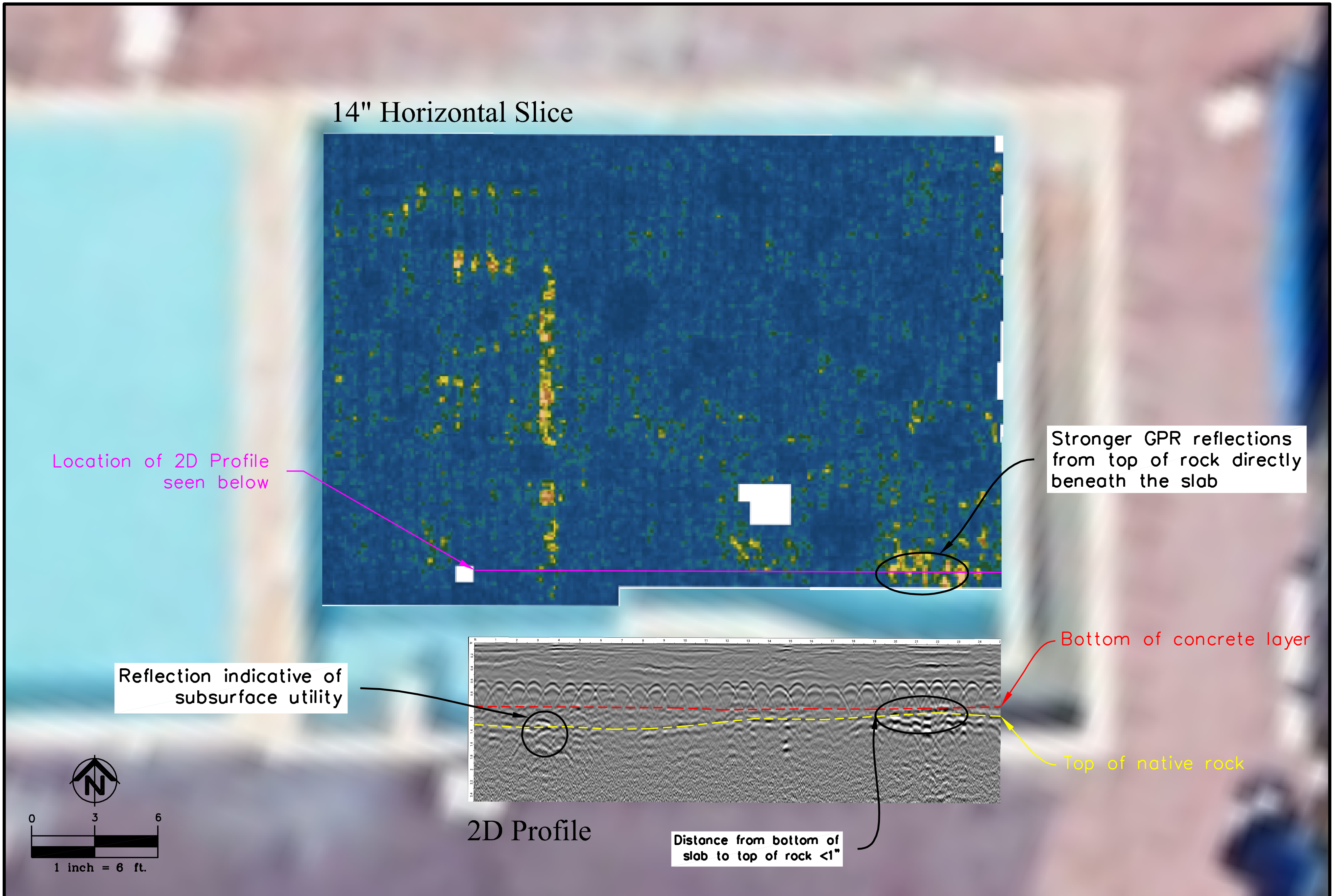
Notes:
1) Project Date: February 3-4, 2026
2) Gehrig, Inc. Project #: 26-10-006
3) GPR data collected with GP8100 antenna

Figure No. 5



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HiRes GPR Vertical Slice Example: East Pool

Highland Horizon Pool - East Pool

Austin, TX 78717

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3) GPR data collected with GP8100 antenna

Figure No. 6

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0 10 20 40
(IN FEET)
1 inch = 20 ft. Horiz.

GPR - 2ft. Depth Slice

Highland Horizon Pool
Austin, Texas 78717

Project #: 26-10-006
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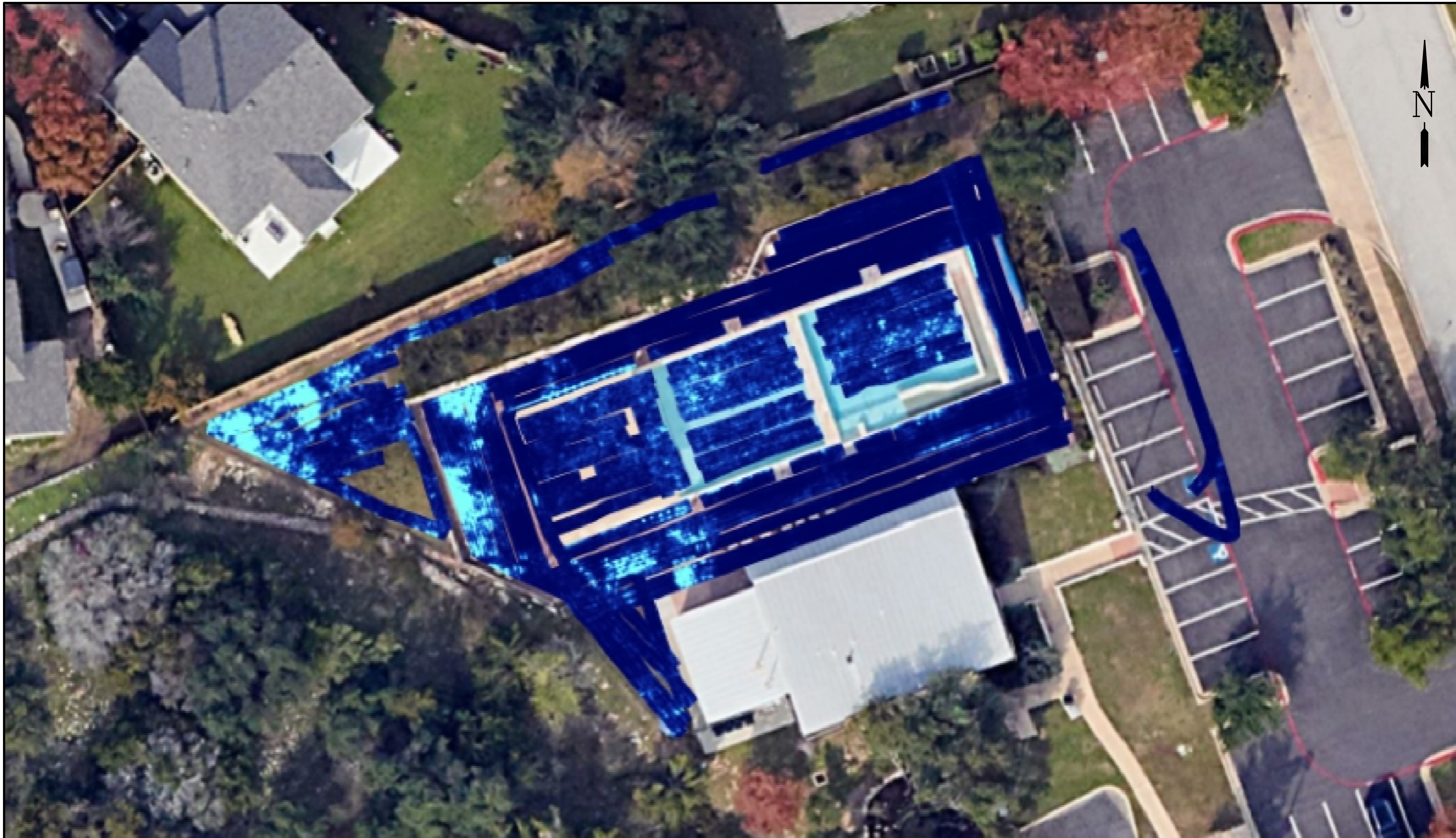
Notes:
1. Aerial: 2013 Google Imagery
2. Datum: State Plane Nad83 - TX Central, ft

Figure No.
7



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0 10 20 40
(IN FEET)
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GPR - 4ft. Depth Slice

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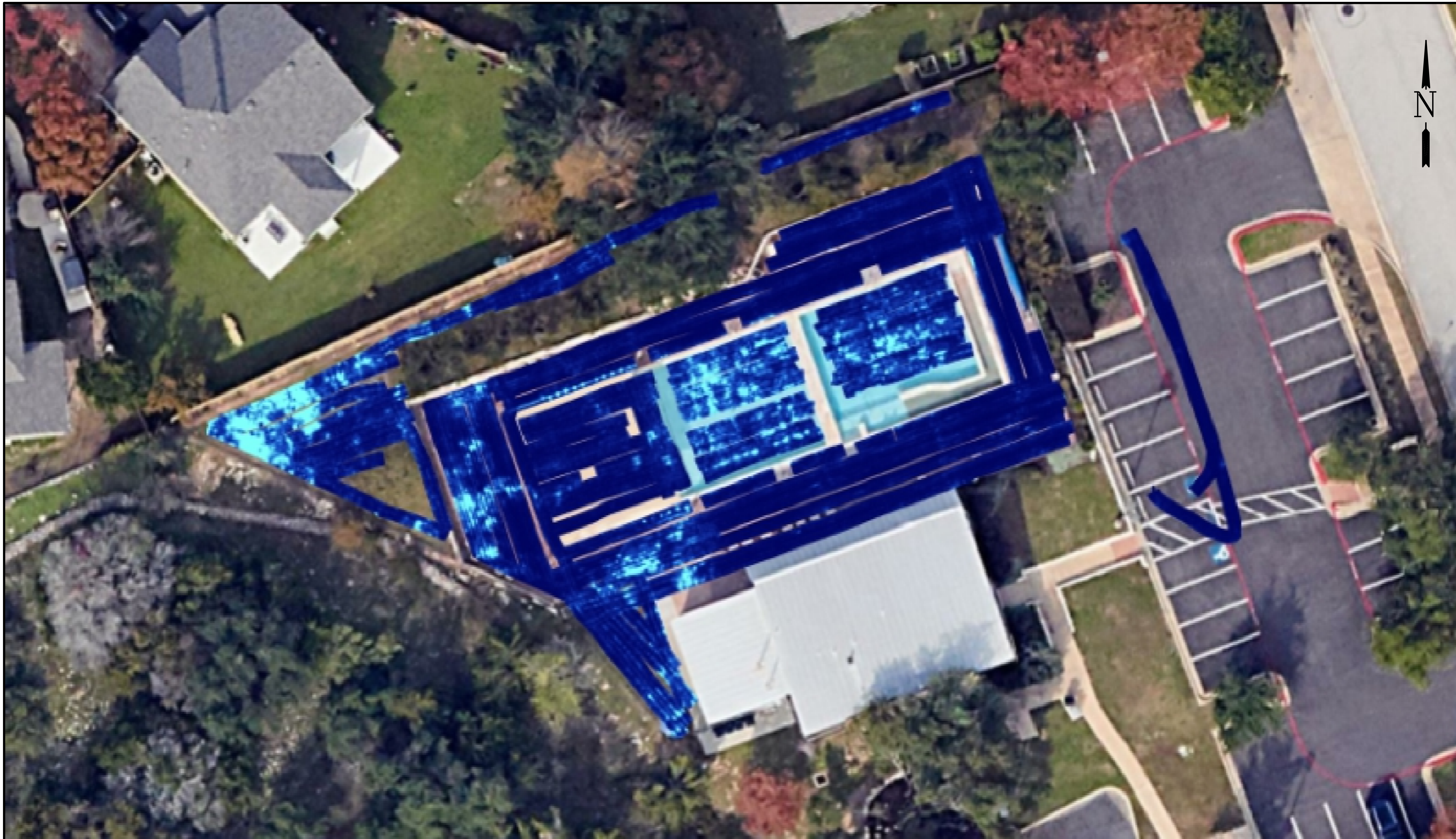
Notes:
1. Aerial: 2013 Google Imagery
2. Datum: State Plane Nad83 - TX Central, ft

Figure No. 8



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0 10 20 40
(IN FEET)
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GPR - 6ft. Depth Slice

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Figure No.
9

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(IN FEET)
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GPR - 8ft. Depth Slice

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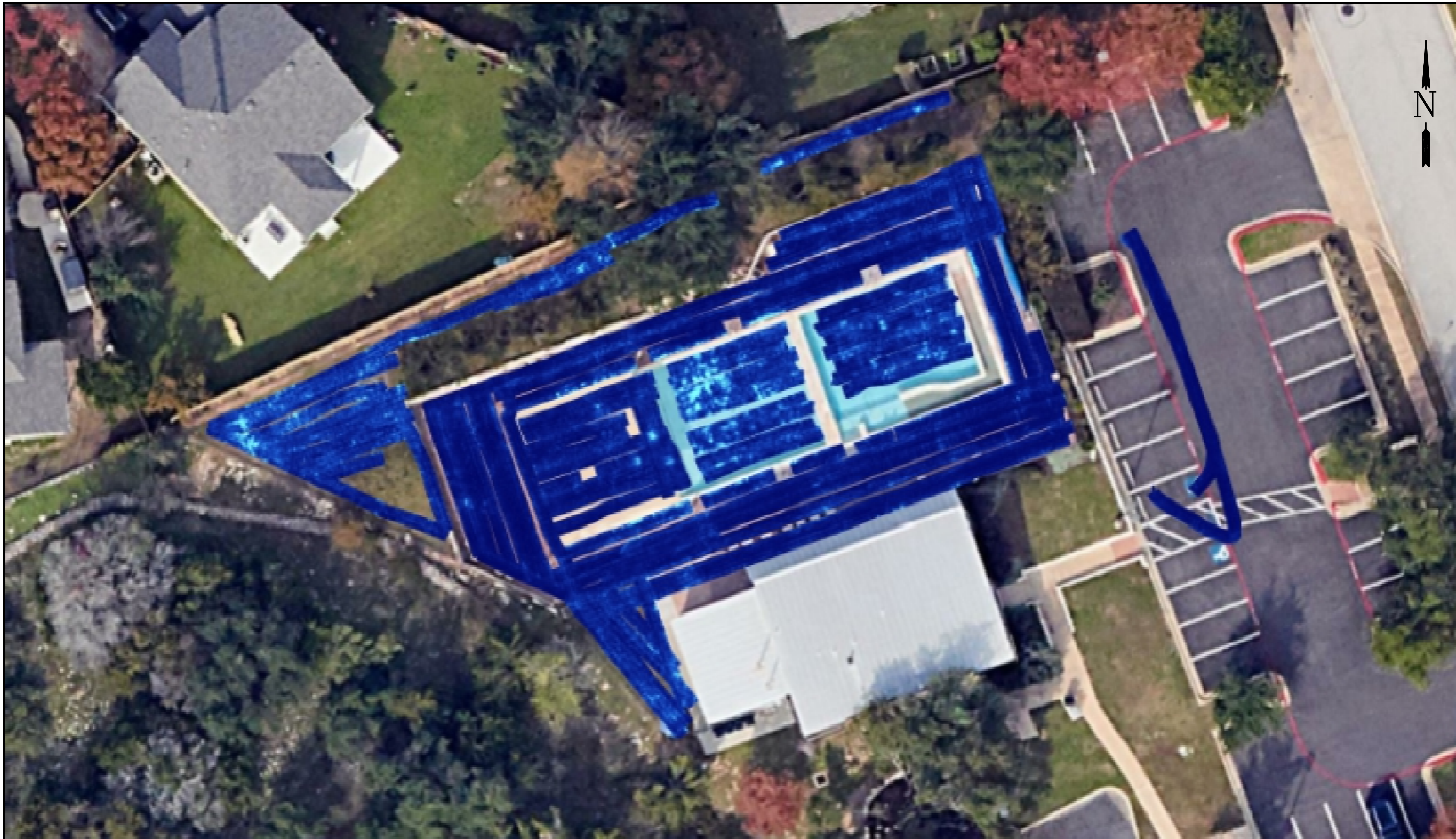
Figure No. 10



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GPR - 10ft. Depth Slice

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Figure No.
11